# Response of Clay Shale to the Variation of Moisture Content

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## **RESPONSL** OF CLAY SHALE TO THE VARIATION OF MOISTURE CONTENT

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NBS! RA((7): 1) therein. If the shale (1) the ocurs in open mining activity because the material is exposed to climate change "-hidt causes righting, Cliange in moisture content and weathering process. Furthermitty, the dumping of excavated material caused an accumulation of water and sounding, at the intermediate layer and further reduced the shear strength. The increase of water content beyond the infiltration capacity will cause the reduction of inter-particle bonding as "ell as cohesion of the shale. This, research focuses on the effect of water content and creep on both exposed and dumped shale. Direct shear test performed on unlighted on samples obtained at random from dumped area confirmed that the change in water content significantly all created on samples obtained at random from dumped area confirmed that the change in water content should be based on the actual shear strength of both the shale and the dumped material.

Kt!)"#"3rd5: shear sirength, clay shale, moisture content, slope stability

### I. INTRODUCTION

Excavation process invoiced in open coal mining activity Cilles. Se exposure of Original shale material to atmosphere and climate charges. This weathering process will bring about the change of the material characteristics from rock to coll. For generical initial engineers, this could be translated to the change in shear strength deterioration. The shear strength and the compressive strength will drastically drop to lowitz value; dud to "eathering.

Increase in water content has been identified as the Jomina"t factor cau; ong the kN of the shear strength of soil and weak reful. This is dee to the abention of coil state from unsaturated to "alurated condition and beyond in "hid, soil looses il's shear strength, especially by the reduction of cohesion. The shear strength of the weathered clay-shale may drup to about 33 \$6 front that of the fresh one. Large amount of infiltration due to rainfall and pounding-water has been identified as a cause of increasing water content. The shear strength will further reduced once the soil is subjected to wetting and totally lo'i, upon saturation. The mechanism of strength loss due to soaking was discussed by Stark and Duncan (1991).

Besides the loss of shear strength, the change of water content and contributes to swelling and shrinkage of soil vohnne. Shrinkage or creep of the suil during dry periods after prolonged wet-and-dry cycles lead to the development

and a starting

Aftension cracks on the surface of a sloping land. During wet seasons, large amount of water infiltrated through the tension cracks and further seeped into the soil layer. The presence rif tension crack initiates 2 sopa; e pattern different from tracs: predicted based on the vriginal slope geometry and soil properties.

This paper summarizes research done at Air Laya open Coal Mining area in South Sumatra, Indonesia (Figure 1). Air Laya is one of several mining sites under the auspices of the Bukit Asam Coal Mining Company Indonesia

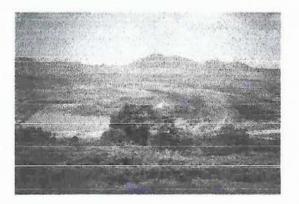


Fig. 1 View of Air [.a)/a open coal mining site

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An open coal mining act/Mfy involves excavating soil to expose ili., coal layer and dumping the excavated overburden soil to an assigned dumping site. The subsurface of Air Laya mining site comprises shale and clay shale material. [bis material is very' hard when dry but hight; cohesive thfCil wet, During, the rainy season, the soil can absorb a large amount of water and because the permeability of the soil is very low, then the Water cannot disvipate easiby. The soil supposed to swell due to the accumulation of water, bin since the scienting, pressure in the soil is very long, the soil turn to become very sticky. The soil condition made the mining activity very difficult especially during we; season (Kramadibrata, 1999).

The total area is, 12:10iia which currently consists of 560IIa mining area and 6:10Ha dumping sites. There art to,o dumping tire, ninicl) speeder 701 and Spreader 702. The excavation is performed by Bucket Wheel Excavalor (BWL). The depth of excavation is 100m with almost vertical angle. The maximum height of fill is 80 m with stepping ll-eight of 8 to 10 m and slope of 1: UH to 1:3H.

Like an) other areas in tropicel region. Air Laya experiences distinctive climatic changes throughout the year. In general, wet weather condition is dominated by North-fast monscon occurs from November to April. The mean annual rainfall for the area is 3,030mm, of which approximately 68.5% fill during wet season. The average ambient temperature is 27°C. 11 e evaporation is limited by high relative humidity, which is about 75% (Gofar *et al.*, 4003).

When the excavated material is  $dtnl \diamondsuit d$  on the dumping area, the sofi i) not compacted and consolidation is expected occur naturally due to the Vieight of fill. During wet season, rainfall will infiltrate into the soil, causing seepage in fill soil and accumulation of water in the intermediate latter between the original soil and the dumped soil, increase of water content beyond inc infiltration capacity Will cause the reduction of inter-particle bonding as well as cohesion of the soil (Rahardjo *et al.* 2000). In this case, the process occurred at a depth below the ground surface therefore, it is not easily detected.

Slope failures and landslides are common in Air Laya, Most of the slope failures and landslides occurred at the end of wet season. The largt"t landshide on dumlping area, occurred in Tolemlar 20-90, was believed to be naused hj/ the development of tension crack on the surface (Gofar, 2006). Frum be standpoint of soil strength, the end of wet season is considered as critical because the soil suction which contributes to the thear strength is minimized or eliminated (Fourie, 1996). Infiltration of rainwater into soil will increase the moisture content of the soils, alter me structure of onls and thuy reduce or eliminate frictional and cohesive strength. Zhang  $eT ul_e$  (2005) proposed a relationship between unconfined compression strength of soil with water content. This research is focused on the evaluation of soil behavior at Air Laya coal mining site and the effect of both creep and the change of water content on the shear strength of clay shale in the dumping area. The understanding un the behavior and the accurate estimation of shear strength is important in the slope stability evaluation.

### 1. METHODOLOGY

The methodology adopted for this study involved the determination of soil index properties and mineralogy as "ell a, chemical content of the soil found in tilt dumping area of Air Laya Coal mining. Determination of these characteristics is important to the comprehension on the actual behavior of the soil. Soil properties tests were conducted on samples collected at the dumping site. All hists were performed following the standard: procedure suggested by ASTM standards 'ASTM, 19'15'). Mineralogy of the soil was evaluated by x-ray test. Chemical composition was evaluated through gravimetry/ spectrofotometry test.

In absence of laboratory equipment to evaluate SWCC curve, the water retention ability of the soil was evaluated  $b\psi$  infiltration and permeability test on falling head permeameter. Infiltration test was performed prior to permeability test and the result was plotted as cumulative infiltration versus time (Green Ampt).

Effect of creep on shear strength was studied ba\Cd on creep test (Rivai, 2003). The let us performed let divert those call of the strength was performed let divert the strength with the strength of the strength of the strength of the strength versus time of failure.

Direct shear tests were performed on 5amples collected at random (III temts of time and location) in the dumping area to e, aluate the relationship between the sh, ar strength and water content. In addition, CBR test was performed on ,both compacted and uncompacted samples to observe the effect of soaking on \$hear strength.

### 3. RESULTS AND DISCUSSION

### 3.1 Soil In<le, Properties and Composition

This classification test indicated that this soil can be grouped as hills plasticity clay or silt (CH or MiH). If should be noted that even though the woulds of Atteberg limit tests indicate that the soil is of high plasticity, the amount of soil passing No. 200 sieve is very low (12.3 196) and the amount of colloid is also low (2.35%). This condition explains the behaviour of soil as described in previous parkgraph. Aclivity of the soil can be computed based on plasticity index and the percentage of colloid. For  $\lambda$  ir Laba soil, the activity is very high i.e. 17 which explain the rapid change in the response of soil to Water. The properties of the soil are sununariled in rable 1.

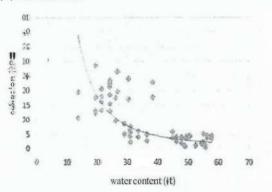
Soii parameter	
Sper."ifK gra∖v <i>itv</i> C"IHBp,osition	2.34
Pastur dese Vu 40	78.14%
porng Xieve on 200	12.31%
5elloid (C < 0.002 mni)	2.35%
LL. (Libuid Intib	65.14%
PLI Plastic Linuit	25.24%
PI (Pi.telicit; insk., )	46%
SL (Shrink); Lintio	i2.°0
SR (Librini ro Rhuio	1.67
ACtiVit#	17
Cossification (ASDI/(TS)	СЦ

The nineralogy of the soil, evaluated by X-Ra) test, showed that the clay is dominated by montmorillonite t-iL5if6), kaolinite 33....00, Siderite (5.2000) and Alpha Quartz (00.20%). The chemical composition is dominated by SiO<sub>4</sub> (5306) and Al<sub>2</sub>O<sub>2</sub> (17?0) hence, the ion exchange capacity from SiO<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub> (17?0) hence, the ion exchange capacity from SiO<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub> (17?0) hence, the soil can be classified as expansive clay which explains the ability of the soil to absorb a large amount of water.

The results of infihration-permicability test shows that the response of the soil it, the increase of water content is very rapid , ithin the first five minutes, bowever the water content at saturation 46.15% was only reached after 1:13 minutes. The volumetric water content at this condition j., 52%. Permeability test was performed upon reaching the saturation and the result shows that the permeability of soil in the dumping site Air laya is 1.3% JO m/s. This shows that the zoil has very low permeability. The Trisults indicate that the zoil bas a large water retention ability and the findings explain the unique response of the soil to wetting during the excavation, transporting and dumping process. As a fill material, the soil was not compacted to rainfall infihration.

### 3.2 Effect of water on shear strength parameter

The effect of vater content on the shear strength parameters was evaluated by doing direct chear test on samples collected at random (in terms of time and place) from the dumping site. The results shown in Figure 3 indicated that even though the data was 'CJ' scattered, then! is a tendency that the shear ctrength in terms of cohesion is affected by water content. The scattering of data is due to the heterogeneity of the material found in the dumping area. The cohesion decreases as the water content increases. At saturated water content, the cohesion decreases to as low as 4 kPa. The results also show that water content has very thall effect on friction angle  $\Rightarrow$  long a" the Wdhr content is 105 than saturation.



rig. > Fffect of \"31/r content on cohesion

Figure 4 shows the results of direct shear test on samples at normal water content (about 2001) and at water content near saturation (about 46%).

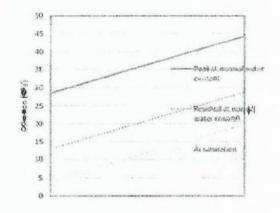


Fig. 4 results of Direct shear test on sample at normal water content and at saturation

Standard Proctor Compaction tests were performed on the soil to evaluate the response of the soil upon soaking and the results shows that the maximum dry density of 16.1 [[N/m] was achieved at an optimum water content of 17%. For compacted soil, the CBR unsoaked and soaked tests were conducted at the optimum water content results in a CBR unsoaked value of 31% and CBR soaked value of 0.8510 with swelling volume of only 0.5100. For soil

prepared at -octer content less than optimum, the CBR unsoaked and tBR soaked are +t06 and 0.49%, respectively with the cliin, volume of 1.65%. The swelling pressure was very low i.e. 0.2 ,Pa. It can be seen that he soil has almost no strength upon &laking especially if the soil is not compacted.

### 31 Free or cristp on shear strength parameter

The efficient of e-Vep on shear strength parameters were etu, Ji-y by eroop hist Figure shows the effect of creep on shear  $\pm t + n_{\rm eff} \ge 1$  under three different normal stresses. The figure choose that the shear strength after creep for about 100 days We about 288 kPa as compared to this average original shear strength of 551 LPa. Extension of the logarithmic curve based on these data shows that the shear strength over a long, period of time was about 400% of the original strength.

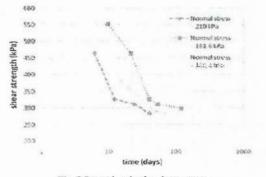


Fig. 5 Strength reduction due to creep

### 3. co::;c;\_\JSJO;\S

The study chockined the unique response of clay shale material obtained in Air Laya mining area to the change in moisture contert. The mineral content of the ciall cause the soil to absorb a large amount of \\cter and become sticky. However the lativ "\\Cling pressure made the soil to break up upon -aturcion and become nucl. This has caused the Jiff@ully in the minin@ activity.

Creep indittel I: the Malation of shiar tirchyth of shale material by as much in 60% while this increase in Water content further reduces the cohesien. Infiltration of water beyond hitturation results in the total loss of strength.

### ACKM!WLL'x;P,HNTS

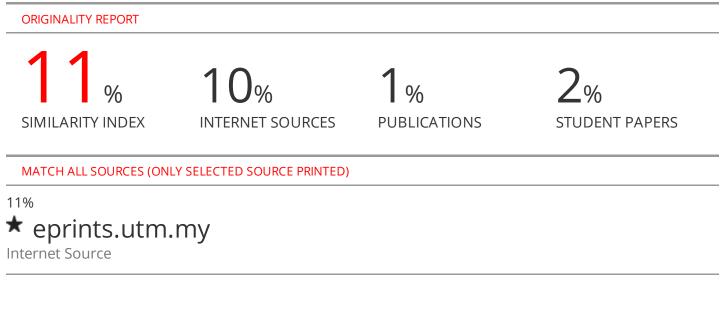
The authors would like to Mpress their p-atitude to PT. Tamhang Batubara Bukit asam Per-ero, Tanjung Enim and Sriv-ijaya University Research Team for permission to use the data for analysis.

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