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Behaviour of Composite Beam with Trapezoid Web Profiled Steel Section in Sub-Assemblage Frame

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Behaviour of Composite Beam with Trapezoid Web Profiled Steel Section in Sub-Assemblage Frame

S. Anis^{1,a}, M. M. Tahir^{2,a}, S. Arizu^{2,b}, P. N. Shek^{2,c}, C.S. Tan^{2,d}, A.B.H. Kueh ^{2,e}

Civil Engineering Department, Faculty of Engineering, Sriwijaya University, Indonesia1

Steel Technology Centre, Universiti Teknologi Malaysia, 81310 UTM Skudai, Johor²

anissaggaf@yahoo.com, mahmoodtahir@utm.my^{2,a}, arizu@utm.my^{2,b}, shekpoingian@utm.my^{2,c}, tcsiang@utm.my^{2,d}, kbhamad@utm.my^{2,d}

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Introduction

The use of the composite and non-composite connections in the design of composite beam with TWP section influenced the maximum moment and the deflection of the beam. However, the extent of the difference is yet to be established. This paper will proposed a method to predict the moment resistance of the composite beam in sub-assemblage frame as a result of connections' restrained. Studies on partial strength or semi-rigid connections have been carried out by many researchers. Shi et al. [1] tested composite joints with flush end plate connection as partial strength connection under cyclic loading. The composite joints with flush end plate connection showed large strength resistance and good ductility, and the slippage between the concrete slab and steel beam was very small, which showed that between the concrete slab and steel beam, full interaction could be obtained by proper design of shear connectors. Studies on the partial strength connection were also carried out by Saggaff [2] and Sulaiman [3]. A series of non-composite connections comprising of flush and extended end-plate connections was tested and compared with composite connection. The beam sections were a built-up section known as trapezoid web profiled steel sections whereas British Sections were used as columns. It was concluded that the moment resistance and the initial stiffness for composite connection were higher than the non-composite connection. Further study on the partial strength connection with TWP steel section was carried out by Tahir et al. [4]. Two full scales testing with beam set-up as sub-assemblage and beam-tocolumn connections set-up as flush and extended end-plate connections were carried out. It was concluded that the use of extended end-plate connection had contributed to significant reduction in the deflection and significant increase in the moment resistance of the beam than flush end-plate connection.

Trapezoidal web profiled steel sections

TWP is a built-up steel section comprised of two flanges connected to a thin corrugated web usually between 3 to 8 mm thick by fillet welding. The web is corrugated at an angle of 45 degree and welded to the two flanges using automated welding machine. The web and the flanges comprised of different steel grade depending on the design requirements. TWP section is also classified as a hybrid steel section with two different types of steel grade welded together to form the section. The steel grade of the flanges is designed for S355 and the steel grade of the web is designed for S275. The flanges are purposely designed for S355 for maximum flexural resistance and the web is designed for S275 so as to reduce the cost of steel material. The shear capacity and bearing capacity are usually not that critical in the design of the beam as the web is corrugated.

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Civil Engineering Department, Faculty of Engineering, Sriwijaya University, Indonesia1

Steel Technology Centre, Universiti Teknologi Malaysia, 81310 UTM Skudai, Johor²

anissaggaf@yahoo.com, mahmoodtahir@utm.my ^{2,a}, arizu@utm.my^{2,a}, shekpoingian@utm.my^{2,a} tcsiang@utm.my2.4, kbhamad@utm.my2.4

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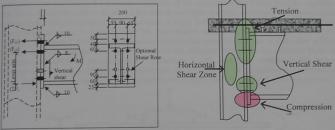
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Test specimen and procedures

The proposed sub-assemblage tests were comprised of three specimens. Each specimen consists of a beam of TWP section connected to the column by the proposed connections as shown in Table 1. The extended and composite connection used are shown in Fig. 1(a and b). No. top bolt row for flush end-plate connection. Details of the geometrical configuration of the sub-assemblage tests are presented in Table 1. The applied load was positioned at the centre of the beam and converted into two point loads by a beam spreader at a distance of 2.1 m as shown in Fig. 2. An increment of about 5 kN was applied to the specimen. The readings of the applied load, displacement, and rotation were recorded after two minutes had elapsed so as to reach an equilibrium state. The incremental load procedure was then controlled by deflection increments of 3 mm. The test was continued until failure, when large deformation or the load decreases significantly. A graph of moment versus rotation was plotted to predict the moment resistance of the connection. The rotation of the connection was measured as the difference between the rotation at the centre of the beam and the rotation at the centre of the column that recorded using inclinometer.



a) Extended end-plate

b) Composite connection

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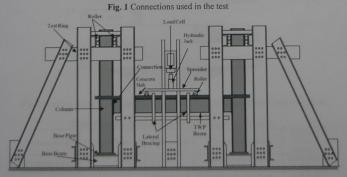


Fig. 2 Test rig for the sub-assemblage tests

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Moment resistance of composite beam

The design of composite beam is based on BS 5950: Part 3.1[5]. Full shear connecters are used in the tested composite beam specimen. Based on the design using BS 5959: Part 3.1, the moment, resistance of the beam MD is calculated as 497.0 kNm. To predict the moment resistance of the composite beam, the moment resistance of the connection in sub-assemblage frame needs to be established first. The moment resistance of the connection can be established by superimposing the rotation of the connection as maximum moment occurred in sub-assemblage frame to the moment versus rotation curves plotted from the isolated tests as presented elsewhere [2, 6]. The predicted moment resistance of the connection is used in the bending moment diagram calculation to predict the maximum moment resistance of the beam in the sub-assemblage test as shown in Fig. 3 and the results are tabulated in Table 2. The results show that the design moment of the beam agrees well with the free bending moment developed from the tested specimens as the ratio is very close to 1.0. The results also show that as the moment resistance of the connection increases the maximum moment at mid-span decreases. Specimen with composite connection tends to reduce the mid-span moment of the beam as the connection is stiffer that the non-composite connection. also show that the higher the moment resistance of the connection the higher the load capacity of the beam. No cracks failure on top of the slab at mid-span for both composite and non-composite specimen in sub-assemblage frame. However, a slight deformation of end-plate in non-composite connections occurred in tension zone. No deformation occurs on the corrugated web of TWP section. Specimen 1 with flush end-plate connection has recorded 30.0mm of deflection at 395kN of maximum load whereas specimen 2 with extended end-plate connection has recorded 34.0mm of deflection at 464kN of maximum load. Specimen 3 with composite connection has recorded 35.0mm of deflection at 477 kN. This shows that the stiffening of the connection has contributed to lesser deflection; however not that significant between flush and extended end-plate connection.

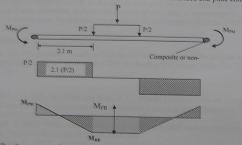


Fig. 3 Bending moment diagram used to predict moment resistance of composite beam

Model Name	Beam Size	Column Size	Connection Types	Bolt Row (Top- Bottom)	
CF2R20P200-12			Flush end-plate (non- composite)	(4-4) M20 8.8	
CE3R20P200-12	450x160x50.2/12/4	305x305x118 (UC-S275)	Extended end-plate (non-	(6-4) M20 8.8	
CFR2R20P200-			composite)		
12			(composite connection)	(4-4) M20 8.8	

able 1 Details of specimens for the sub-assemblage tes	able 1 De	ans or	specir	nens	tor	the	sub-asser	mblag	test
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Specimen Name	Maximum Load, (kN)	Free Bending Moment M _{FB} (kNm)	Ratio of M _{FB} /M _D	Moment At Connection M _{PM} (kNm)	Moment At Mid-Span, M _{RB} (kNm)	Deflection At Max. Load (mm)
Specimen 1 (non-comp. connection)	395	415	1.12	135	280	30
Specimen 2(non-comp. connection) Specimen 3	464	487	1.02	205	282	34
(composite connection)	477	501	0.99	320	181	35

Table 2 Test results from the Composite Full-Scale Sub-Assemblage tests

Conclusions

The concluding remarks from the experimental results of the proposed connections are as follows:-

- The use of composite connection and extended end-plate connection has significantly reduced the deflection of the beam and increase the loading capacity of the beam. The significant increment in the stiffness of composite connection and extended end-plate connection however has not developed any failure on the column section which concludes that no stiffener is needed.
- The results show that the higher the moment resistance of the connection the higher the load capacity of the beam.
- 3) The results show that the design moment of the beam agrees well with the free bending moment developed from the tested specimens as the ratio is very close to 1.0.
- 4) No cracks failure observed on top of the slab at mid-span for the composite specimen in subassemblage frame. However, a slight deformation of end-plate in non-composite connections occurred in tension zone. No deformation occurs on the corrugated web of the TWP section.

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