Exergetic Analysis sustainability Index (ESI) On Gas Turbine Compressor Package (GTCP) At Pt. Pertamina Gas Negara (PGN) Pagardewa Station By Agung Mataram

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Abstract:

Gas Turbine Compressor Package (GTCP) adalah turbin gas berfungsi sebagai penggerak kompresor sebagai beban dimana kompresor ini berfungsi untuk menaikkan tekanan gas sehingga gas tersebut mampu dialirkan menuju unit-unit penerimaan gas. Untuk mendapatkan hasil optimal dalam pengoperasian GTCP diperlukan analisis terhadap parameter-parameter yang berpengaruh didalam sistem GTCP, dimana dalam hal ini parameter yang berpengaruh tersebut adalah rasio kompresi pada kompresor. Pada penelitian ini digunakan analisis exergy untuk dapat mengetahui kerugian exergy pada kondisi operasi disetiap sub-sistem pada GTCP. Setelah melakukan analisis exergy pada kondisi operasi kemudian dilakukan modifikasi pada parameter rasio kompresi untuk dapat mengetahui hubungan antara rasio kompresi dengan eksergi yang dimusnahkan, efisiensi exergetic, dan kerja bersih GTCP, dimana dalam hal ini modifikasi rasio kompresi adalah senilai 16,5:1 sebagai model A yang merupakan rasio kompresi desain ,9:1 sebagai model B yang merupakan rasio kompresi dibawah kondisi operasi dan 13:1 sebagai model C yang merupakan rasio kompresi diatas kondisi operasi. Setelah didapat hasil analisis exergy pada kondisi berbagai permodelan tersebut dilakukan analisis Exergetic Sustainability Index (ESI) sehingga didapat nilai rasio tekanan yang menunjukan nilai ESI, Environtmental Effect Factor dan Kerja Bersih optimal yaitu pada model C dengan rasio kompresi sebesar 13:1

Key Word: GTCP; Exergy; Rasio Kompresi; Exergetic Sustainability Index; ESI; Environmental Effect Factor.

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I. Introduction

PT. PGN Pagar Dewa Station, which plays an important role in the gas distribution business in Indonesia, has gas turbine equipment as or 6 of the supporting utilities in distributing gas in the transmission pipeline network to all end-use 6 both in the power generation industry, ceramics ind 6 try and other commercial users. PT. PGN uses the gas turbine to drive the compressor in a system called the Gas Turbine Compressor Package (GTCP) to compress gas from the PT. Conoco Philips and PT. Pertamina to Java Island.

For enhancement efficiency with appropriate so needed results capable analysis _ tell availability actual energy (exergy) , losses exergy , causes , as well as the location . Analysis exergetic sustainable index is analysis system thermal in a manner qualitative used _ For measure quality from a process and can applied to the GTCP used by PT. PGN Stations Pagardewa For identify source inefficiency , determine location , and size exergy losses that occur so that can determined condition Work the most optimal equipment .

For condition Work the most optimal equipment in operation GTCP , then need done analysis more indepth on parts of the GTCP as well as do modifications to the operating parameters . Optimization is the process for get conditions , ie values from the variables , which gives minimum values or maximum from function objective

II. Methodology

In this study, exergy analysis calculations will be carried out on the processes in each sub- system in the GTCP and the exergy dissipated into the environment at design and operating conditions as well as dooptimization with give modifications to the ratio compression and temperature especially at the turbine inlet on the GTCPso that got explanation showing connection between ratio compression, turbine inlet temperature, compressor inlet temperature , exergy destroyed , efficiency exergetic , and work net so that the right strategic

steps are obtained to obtain optimum operating conditions that show maximum or minimum function according to needs.

To overcome the limitations caused by the lack of points that are given measuring instruments on the GTCP and situations where the value is not yet known, an analysis of the first law of thermodynamics will be carried out to complete the required data.

To be able to determine the specific enthalpy and specific heat values for each air and gas composition needed in the first law of thermodynamics analysis and exergy analysis in GTCP, a tool is needed in the form of a calculator properties of air and gas as well as a table of properties tool.

Besides completeness of the data, the accuracy of the data is also required when do analysis and optimization exergy on GTCPespecially in the combustion chamber. Therefore, any calculations based on the molar mass composition, whether on the side of the air entering the combustion chamber, fuel, or flue gas resulting from combustion, will usedata from the readings of measuring instruments

Analysis of the First Law of Thermodynamics

The design and operation data obtained from the control room are arranged to be placed at each point on the flowchart so that conditions at each unknown point can be identified. These data are then processed using the Microsoft Excel program worksheet to carry out calculations of the first law of thermodynamics analysis in every unknown condition. Furthermore, the calculated data is arranged in tabular form and then displayed in the form of a T-s diagram. From the T-s diagram, the parameters of temperature and compression ratio are obtained in the design and operating conditions of the GTCP system.

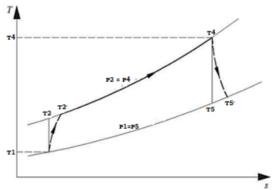


Figure 1. T-s GTCP system diagram of PT PGN Pagardewa Station

Exergy Analysis and ESI Analysis on sub-systems in GTCP

After getting all the parameters needed, the data will be carried out by an exergy analysis process for each sub-system in the GTCP system. The exergy analysis performed on the design and operation data will yield the exergy output at each point and the exergy annihilated for each sub-system and its relationship to work net and compressor under design and operating conditions. The value of the exergy equilibrium rate at GTCP is as follows:

$$[(\dot{E}_{C} - \dot{E}_{DC}) + \dot{W}_{C}] + [(\dot{E}_{CC} - \dot{E}_{DCC})] + [(\dot{E}_{T} - \dot{E}_{DT}) - \dot{W}_{Nett} - \dot{E}_{L}] = 0$$
 (II.1)

After the data from the exergy analysis is obtained, modifications will be made by providing variations on the influential parameters, in this case pressure with the maximum value limit that exists in the manufacturing design data.

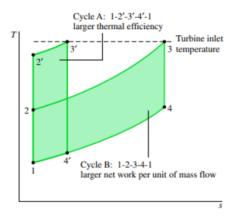


Figure 2. T-s diagram on modification of compression ratio with unchanged turbine inlet temperature (Source: Moran, 2006)

After getting results analysis exergy on each modification variations in the influential parameters the so results modification will made in tabular data form with various modeling . the tabular data Then done ESI for can know influence from modifications to GTCP parameters .

$$\lambda = \frac{1}{\gamma_{Eef}} \tag{II.2}$$

$$\gamma_{Eef} = \frac{\tau}{\eta_{\varepsilon}} \tag{II.3}$$

$$\tau = \frac{\hat{E}_{DTotal}}{\hat{E}_{in}} \tag{II.4}$$

III. Description System

Technical specifications

Table 1GTCP PT PGN Pagardewa Station Technical Specifications

| 1 Description | Information |
|--|---|
| Compressor Type | Axial Flow |
| Compressor number of stages | 14 |
| Compression Ratio | 16, 5:1 |
| Compressor Inlet air flow (nominal) | 26.2 kg/sec (57.7 lbs /sec) |
| Combustion Chamber Type | Annular |
| ignition | Torches |
| Number of fuel injectors | 12 |
| Gas Producer Turbine Type | reaction |
| Number of stages | 2 |
| Maximum speed | 15,200rpm |
| Output Power | 7690 kW (10,300 HP) |
| Heat rate exhaust | 10,340 kJ/kWh (7,310 Btu/kWh) |
| Flow exhaust | 95630 kg/d (210,830 lb /h) |
| Turbine inlet temperatures | 495 °C (920 °F) |
| ignition Number of fuel injectors Gas Producer Turbine Type Number of stages Maximum speed Output Power Heat rate exhaust Flow exhaust | Torches 12 reaction 2 15,200rpm 7690 kW (10,300 HP) 10,340 kJ/kWh (7,310 Btu/kWh) |

Source GTCP Manufacturing data record, Solar Turbines Taurus-70

| Table 2GTCP Fuel System Technical Specifications | | | | |
|--|-------------------------------------|--|--|--|
| Description | Information | | | |
| Gas Fuel System | Natural Gas, Propane | | | |
| Acceptable Gas Fuels | 1 onventional or SoLoNOx | | | |
| Minimum/Maximum Gas Fuel | 1860 to 2760 kPag (270 to 400 psig) | | | |
| Supply Pressure | | | | |
| Minimum Flow rate | 1950 12 hr (4297 lbm /d) | | | |
| Minimum/maximum Fuel Supply | -40 °C to 93 °C (40 °F to 200 °F) | | | |
| Temperature | | | | |
| Maximum Operating Pressure | 3447 kPag (500 psig) | | | |
| Maximum Operating Temperature | 93 °C (200 °F) | | | |

PT PGN's GTCP Operation Data at Pagardewa Station

| Table 3PT PGN's | GTCP Operation | Data at Pagardewa Station |
|-----------------|----------------|---------------------------|
| | | |

| Parameter | units | Mark | |
|-------------------|------------------------|----------|--|
| T ₁ | ⁰ F | 85,20 | |
| T ₄ | $^{0}\mathrm{F}$ | 1391,11 | |
| T 5 | $^{0}\mathrm{F}$ | 219.94 | |
| P ₂ | psig | 150,10 | |
| Flow Compressors | mscfd | 72.54 | |
| T Fuel | 0 F | 110.9652 | |
| P _{Fuel} | psig ⁰ F | 759,2429 | |
| T Sales Gas 2 | 0 F | 103.88 | |
| P Gas Sales 1 | Psig | 1.03 | |

Table 4GTCP Fuel Composition of PT PGN Pagardewa Station

| Type | Percentage |
|------------|------------|
| Methane | 81.2829 |
| Ethane | 5.7772 |
| Propane | 1.3930 |
| i -butane | 0.2678 |
| n-butane | 0.3893 |
| i -pentane | 0.1608 |
| n-pentane | 0.1230 |
| n-hexane | 0.2051 |
| N_2 | 1.2166 |
| CO2 | 9.1146 |
| H2O | 0.0690 |
| H2S | 0.0007 |
| AMOUNT | 100 |
| | |

IV. Analysis and Discussion

Analysis of the First Law of Thermodynamics

The purpose of analyzing the first law of thermodynamics is to complete the operating data that has been obtained during data collection at the research location and as a basis for exergy analysis calculations. Placing the points that become parameters will make it easier to analyze and assist in completing the operating data that has been obtained during data collection at the research location.

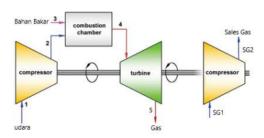


Figure 3 PT PGN Pagardewa Station GTCP flowchart

So that the values obtained from each point in the GTCP system of PT PGN Pagardewa station are as follows.

Table 5. The value at each point in the GTCP system

| | rable 5. The value at each point in the GTCF system | | | | | |
|-------|---|---------|----------|--------------|-------------|--|
| Point | T(0 C) | P(bar) | m (kg/s) | C p (kJ/kgK) | H(kW) | |
| 1 | 29,556 | 1.01325 | 23.77 | 1.005 | 7231,298228 | |
| 2 | 324,407 | 11.362 | 23.77 | 1.05 | 14914,12638 | |
| 2' | 330,723 | 11.362 | 23.77 | 1,051 | 15086,11833 | |
| 3 | 43.8695 | 52.3479 | 1.5 | 2.06 | 979,590255 | |
| 4 | 755,0611 | 11.362 | 25,27 | 0.88441700 | 22979,71378 | |
| 5 | 270.4131 | 1.01325 | 25,27 | 0.87555383 | 12026,46745 | |
| 5' | 299.1191 | 1.01325 | 25,27 | 0.87962735 | 12720,50279 | |

Table 6. The value of each sub-system on the GTCP system

| State | 11 | WorQ(kW) |
|-------------------------------------|-----------------------------|-------------|
| Work Compressor (\dot{W}_C) | H 2-H 1 | 7854,820104 |
| Combustion chamber(Q) | H_{4} - $(H_{2} + H_{3})$ | 6914.005194 |
| Work turbine (\dot{W}_{Turbin}) | H5 - H4 | 10259,21099 |
| Work Nett(W _{Nett}) | $(H_5-H_4)-(H_2-H_1)$ | 2404,390885 |

Exergy analysis on GTCP

The purpose of analyzing exergy in GTCP is For can know exergy values at each point in the GTCP and exergy destroyed in each sub- component in the GTCP.

Table 7.Exergy value at each point in GTCP

| | Table 7.Exergy value at each point in GTC1 | | | | | |
|-------|--|---------------------------|-------------------------------------|--|--|--|
| Point | $\dot{E}_{physics}(kW)$ | $\dot{E}_{chemistry}(kW)$ | $\dot{E}_{physics + chemistry}(kW)$ | | | |
| 1 | 58.50198384 | 0 | 58.50198384 | | | |
| 2 | 7205,755363 | 0 | 7205,755363 | | | |
| 2' | 7367,087275 | 0 | 7367,087275 | | | |
| 3 | 18.31598252 | 70504,34181 | 70522,65779 | | | |
| 4 | 15944,5778 | 1763,158626 | 17707,73643 | | | |
| 5 | 5229,464497 | 1763,158626 | 6992,623124 | | | |
| 5' | 5878,281976 | 1763,158626 | 7641,440602 | | | |

Table 8.Exergy Loss value for each sub- system in GTCP

| Sub- system | | Exergy Loss (kW) |
|--|---|------------------|
| Compressor (Ė _{DC}) | $\dot{W}_{C} - \dot{E}_{2^*}$ | 649.0647404 |
| Combustion Chamber (E _{DCC}) | $\dot{E}_{2^*} + \dot{E}_3 - \dot{E}_4$ | 60182,00864 |
| Turbine (\dot{E}_{DT}) | $\dot{\mathbf{E}}_{5+} + \dot{\mathbf{W}}_{nett} + \dot{\mathbf{W}}_{C} - \dot{\mathbf{E}}_{4}$ | 192.9151628 |
| wasted to environment(\dot{E}_L) | Ė ₅ * | 7641,440602 |

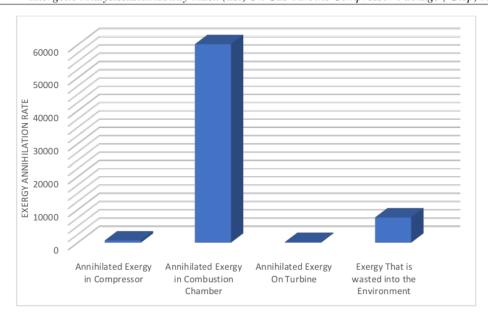


Figure 4 Graph of Exergy Loss Rate at GTCP PT PGN Pagardewa Station

From the chart above, we can see that the GTCP component that has the greatest exergy loss rate is exergy destroyed in the combustion chamber, followed by exergy discharged into the environment through the chimney and then exergy destroyed in the compressor and finally exergy destroyed in the turbine.

Modifications to the GTCP system

Modifications to PT PGN's GTCP Pagardewa station were carried out by providing variations in the compression ratio variable. The compression ratio in the design specifications is 16.5:1 (sixteen point five to one) where in operating conditions the compression ratio can be calculated as 11.2:1 (eleven point two to one). This research was conducted by calculating the compression ratio modeling above and under operating conditions. By modifying the compression ratio parameter with a target that the temperature of the combustion gas entering the turbine is constant according to the operating conditions, the values of each point in the GTCP system of PT PGN Pagardewa station are obtained with various models as follows.

Table 9 Values at each point on the GTCP Model A system with compression ratio conditions according to design

| conditions. | | | | | |
|-------------|------------|-----------|----------|-------------|-------------|
| Point | T(°C) | P (bar) | ṁ (kg/s) | Cp (kJ/kgK) | H (kW) |
| 1 | 29,556 | 1,01325 | 23,77 | 1,005 | 7231,298228 |
| 2 | 390,433469 | 16,718625 | 23,77 | 1,06626003 | 16818,52369 |
| 2' | 401,181713 | 16,718625 | 23,77 | 1,06883961 | 17132,28565 |
| 3 | 43,8695 | 52,3479 | 1,05 | 2,06 | 685,7131785 |
| 4 | 755,0611 | 16,718625 | 24,82 | 0,88441700 | 22570,49846 |
| 5 | 215,116350 | 1,01325 | 24,82 | 0,87026651 | 10546,56046 |
| 5' | 247,966308 | 1,01325 | 24,82 | 0,87434265 | 11308,8413 |

Table 10The value at each point on the GTCP Model B system with a compression ratio under operating conditions

| | | | 18 9:1 | | |
|-------|----------|---------|----------|-------------|-------------|
| Point | T(0 C) | P(bar) | ṁ (kg/s) | Cp (kJ/kgK) | H(kW) |
| 1 | 29,556 | 1.01325 | 23.77 | 1.005 | 7231,298228 |
| 2 | 289.4253 | 9.11925 | 23.77 | 1.042766574 | 13944,3081 |
| 2' | 293.9527 | 9.11925 | 23.77 | 1.043762603 | 14069,95345 |
| 3 | 43.8695 | 52.3479 | 1,7 | 2.06 | 1110,202289 |
| 4 | 755,0611 | 9.11925 | 25,47 | 0.884417007 | 23161,58726 |
| | | | | | |

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| 5 | 304.4327 | 1.01325 | 25,47 | 0.880811034 | 12957,64021 |
|----|----------|---------|-------|-------------|-------------|
| 5' | 330,4521 | 1.01325 | 25,47 | 0.880751401 | 13540,44876 |

Table 11The value at each point on the GTCP Model C system with a compression ratio over operating conditions

| | | | 18 13:1 | | |
|-------|----------|----------|----------|-------------|-------------|
| Point | T(0C) | P(bar) | m (kg/s) | Cp (kJ/kgK) | H(kW) |
| 1 | 29,556 | 1.01325 | 23.77 | 1.005 | 7231,298228 |
| 2 | 348.8766 | 13.17225 | 23.77 | 1.05628638 | 15617,79911 |
| 2' | 356.7774 | 13.17225 | 23.77 | 1.05818259 | 15844,56626 |
| 3 | 43.8695 | 52.3479 | 1,3 | 2.06 | 848.978221 |
| 4 | 755,0611 | 13.17225 | 25.07 | 0.88441700 | 22797,8403 |
| 5 | 248.6593 | 1.01325 | 25.07 | 0.87441908 | 11438,94025 |
| 5' | 278.9724 | 1.01325 | 25.07 | 0.87778062 | 12149,98488 |

By obtaining the value of each point on the GTCP of PT PGN Pagardewa station, a comparison of the T-s diagrams of each model can be made so that through Figure 5 it can be seen that with a change in the compression ratio, there is also a change in other parameters at the PT PGN GTCP station Pagardewa..

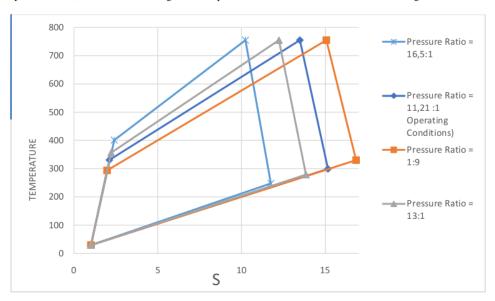


Figure 5 . T-s PT PGN Pagardewa Station GTCP diagram under operating conditions and under modified compressor pressure ratio conditions

Exergy analysis of the results of modifications to the GTCP system

By changing the parameters from the modification of the compression ratio, exergy analysis is then carried out on each model to be able to make a comparison of each model as follows.

| Toblo | 12Exergy values a | t anah naint in | GTCD Model A |
|-------|-------------------|-----------------|--------------|
| | | | |

| Point | Ė _{physics} (kW) | Ė _{chemistry} (kW) | $\dot{E}_{physics + chemistry}(kW)$ |
|-------|---------------------------|-----------------------------|-------------------------------------|
| 1 | 58.50198384 | 0 | 58.50198384 |
| 2 | 8957,22078 | 0 | 8957,22078 |
| 2' | 9246,806109 | 0 | 9246,806109 |
| 3 | 2.677956017 | 49353,03927 | 49355,71722 |
| 4 | 15654,81847 | 1731,760867 | 17386,57934 |
| 5 | 3936,185683 | 1731,760867 | 5667,94655 |
| 5' | 4650,409235 | 1731,760867 | 6382,170102 |

| Tuble ISExergy Boss va | rac for each sao system in GTC1 | TTTOGCT I I |
|--------------------------------------|--|------------------|
| Sub- system | | Exergy Loss (kW) |
| Compressor (Ė _{DC}) | $\dot{W}_{C} - \dot{E}_{2^*}$ | 943.7666431 |
| Combustion Chamber (\dot{E}_{DCC}) | $\dot{E}_{2^{+}} + \dot{E}_{3} - \dot{E}_{4}$ | 41215,94399 |
| Turbine (Ė _{DT}) | $\dot{\mathbf{E}}_{5} + \dot{\mathbf{W}}_{nett} + \dot{\mathbf{W}}_{C} - \dot{\mathbf{E}}_{4}$ | 257,2479203 |
| wasted to environment(\dot{E}_L) | Ė ₅ + | 6382,170102 |

Table 14.Exergy values at each point in GTCP Model B

| Point | Ė _{physics} (kW) | Ė _{chemistry} (kW) | $\dot{E}_{physics + chemistry}(kW)$ |
|-------|---------------------------|-----------------------------|-------------------------------------|
| 1 | 58.50198384 | 0 | 58.50198384 |
| 2 | 6307,931266 | 0 | 6307,931266 |
| 2' | 6423,770014 | 0 | 6423,770014 |
| 3 | 25.26621652 | 79904,92072 | 79930,18694 |
| 4 | 16073,35973 | 1777,113186 | 17850,47291 |
| 5 | 6050,892224 | 1777,113186 | 7828.00541 |
| 5' | 6622,513179 | 1777,113186 | 8399,626365 |

Table 15Exergy Loss Value for each sub-system in GTCP Model B

| Sub- system | | Exergy Loss (kW) |
|---|--|------------------|
| Compressor (Ė _{DC}) | $\dot{W}_{C} - \dot{E}_{2^*}$ | 530,7239509 |
| Combustion Chamber (\dot{E}_{DCC}) | $\dot{E}_{2^*} + \dot{E}_3 - \dot{E}_4$ | 68503,48404 |
| Turbine (Ė _{DT}) | $\dot{\mathbf{E}}_{5} + \dot{\mathbf{W}}_{nett} + \dot{\mathbf{W}}_{C} - \dot{\mathbf{E}}_{4}$ | 170.2919478 |
| wasted to environment(E _L) | Ė ₅ + | 8399,626365 |

Table 16Exergy values at each point in GTCP Model C

| | rable rouncing values at | eden ponk in or er wie | raci c |
|-------|--------------------------|---------------------------|-------------------------------------|
| Point | $\dot{E}_{physics}(kW)$ | $\dot{E}_{chemistry}(kW)$ | $\dot{E}_{physics + chemistry}(kW)$ |
| 1 | 58.50198384 | 0 | 58.50198384 |
| 2 | 7850,54626 | 0 | 7850,54626 |
| 2' | 8059,358606 | 0 | 8059,358606 |
| 3 | 11.36574852 | 61103,7629 | 61115,12865 |
| 4 | 15815,79588 | 1749,204066 | 17564,99994 |
| 5 | 4713,962978 | 1749,204066 | 6463,167044 |
| 5' | 5384,269777 | 1749,204066 | 7133,473843 |

Table 17 Exergy Loss Value for each sub-system in GTCP Model C

| Table 17 Exergy 2000 value for each sub-system in G1 C1 Model C | | | | |
|---|---|------------------|--|--|
| Sub- system | | Exergy Loss (kW) | | |
| Compressor (Ė _{DC}) | $\dot{W}_{C} - \dot{E}_{2^*}$ | 762.7217668 | | |
| Combustion Chamber (\dot{E}_{DCC}) | $\dot{E}_{2^*} + \dot{E}_3 - \dot{E}_4$ | 51609,48731 | | |
| Turbine (Ė _{DT}) | $\dot{E}_{5+} + \dot{W}_{nett} + \dot{W}_{C} - \dot{E}_{4}$ | 216,3293246 | | |
| wasted to environment(E _L) | Ė ₅ + | 7133,473843 | | |

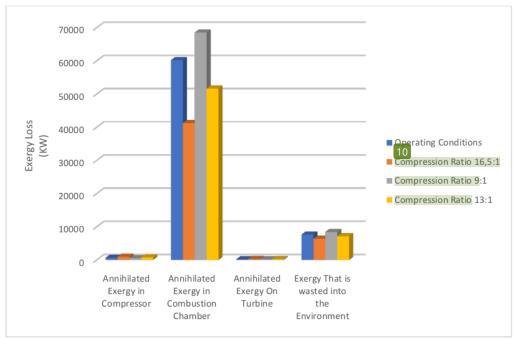


Figure 6 T-s Graph of Exergy Loss Rate for each model at GTCP PT PGN Pagardewa Station

Exergetic Sustainability Index (ESI) analysis on GTCP

From the results of the exergy analysis under operating conditions and various modification models to PT PGN's GTCP Pagardewa Station, an ESI analysis is carried out where the higher the ESI value, the smaller the reduction in resources, be it reductions in fuel use, man-power, and so on. In addition, environmental effect calculations will also be carried out, where the environmental effect factor shows the level of environmental damage caused by exergy losses in a system. The lower the value of the Environmental Effect Factor, the lower the level of environmental damage, but the greater the unit cost needed to achieve it.

| Table 17Exergetic Sustainability Index (ESI) analysis on GTCP | | | | | | |
|---|----------------------------------|-----------------|----------|--------------------|----------------|---------|
| Condition | $\dot{E}_{DTotal} + \dot{E}_{L}$ | Ė _{in} | τ | $\eta_{arepsilon}$ | γ_{Eef} | λ |
| Operation | 68665,42915 | 113770,0146 | 0.603545 | 0.10752 | 5.61308 | 0.17815 |
| Model A | 48799,12866 | 97210,24924 | 0.501995 | 0.16492 | 3.91803 | 0.25522 |
| Model B | 77604,1263 | 120722,7256 | 0.642829 | 0.10435 | 6.16001 | 0.16233 |
| C model | 59722,01225 | 106059,1126 | 0.563101 | 0.11576 | 4.86418 | 0.20558 |

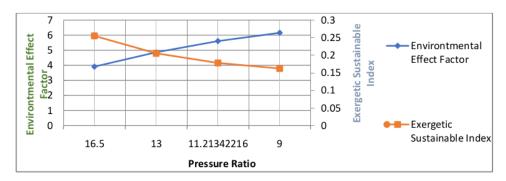


Figure 7. Relationship between ESI and Environmental Effect Factor with Compression Ratio at PT PGN Pagardewa's GTCP

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The ESI value which is an indicator in the Quality of a process must also be related to the output power in terms of PT PGN Pagardewa's GTCP is Work Net(\dot{W}_{nett}) to drive the compressor as a load to distribute gas to customers, where the relationship between ESI and Net Work is detailed in the table following.

| Table 18Relationship between ESI and Net Work (\dot{W}_{nett}) | | | |
|--|-------------------------|---------|--|
| Condition | \dot{W}_{nett} (kW) | λ | |
| Operation | 2404,391 | 0.17815 | |
| Model A | 1360.67 | 0.25522 | |
| Model B | 2782,483 | 0.16233 | |
| C model | 2034,587 | 0.20558 | |

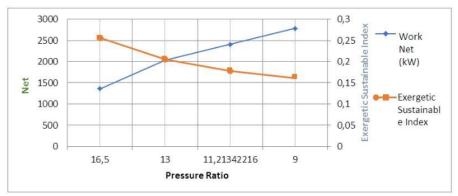


Figure 8. Relationship between ESI and Work Netwith Compression Ratio at PT PGN Pagardewa's GTCP

V. Discussion

Conclusion

Based on the results of processing operating condition data obtained from the control room of PT PGN Pagardewa station and modification of the compressor pressure ratio, it can be concluded:

- 1. The greater the compression ratio, the higher the ESI value which indicates that the better the quality of the ongoing process.
- 2. The greater the compression ratio, the lower the value of the environmental effect factor which indicates that the less environmental damage occurs due to exergy losses in the system.
- With the ESI analysis of the modified modeling of the compression ratio parameter, the optimal pressure ratio value which shows the ESI value, Environment Effect Factor and optimal Clean Work is 114 del C with a pressure ratio of 13:1.
- 4. The results of the exergy analysis show that the largest exergy losses in each model occur in the combustion process in the combustion chamber followed by exergy losses to the environment.
- 5. The exhaust gas in GTCP which is lost to the environment through the chimney still has a large enough exerg 9 value to be reused either as a pre-heater before entering the combustion chamber, you can also use a WHRB (Waste Heat Recovery Boiler) or HRSG (Heat Recovery Steam) Generator.

Suggestion

To get more accurate results in calculations using operating conditions, accurate data is needed so that calibration of the equipment used in measuring operating conditions is required.

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